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# **Development of a Diagnostic System for Air Brakes in Trucks**

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# Acknowledgement

- **NSF/GOALI CMMI 0556343 with Meritor-WABCO.**
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- **Texas Transportation Institute.**
- **Current: Safe-D UTC grant**

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# Outline

- Introduction to Air Brakes
- Main Issues for a diagnostic system for air brakes
- Experimental Setup at Texas A&M University
- Diagnostic Algorithms
  - Estimation of Stroke of Pushrod
  - Detection of Leaks

# Introduction

## ■ Commercial vehicles

- **Transport 23% of freight in the United States**

(Source: US DoT – Bureau of Transportation Stat.)

- **23.5 million children use school buses**

(Source: US DoT – Bureau of Transportation Stat.)

- **9 million HCVs reported in the US in 2006**

(Source: US DoT – Bureau of Transportation Stat. )

- **Heavy commercial vehicles (HCVs)**

- **Gross vehicle weight rating > ~14,000 kg**

- **HCVs require large braking forces**

- **Use air brake system for braking**



# Air Brake System

Front Brake Chambers  
(TYPE 20)

Rear Brake Chambers  
(TYPE 30)

Driver Input

Treadle Valve

Relay Valve

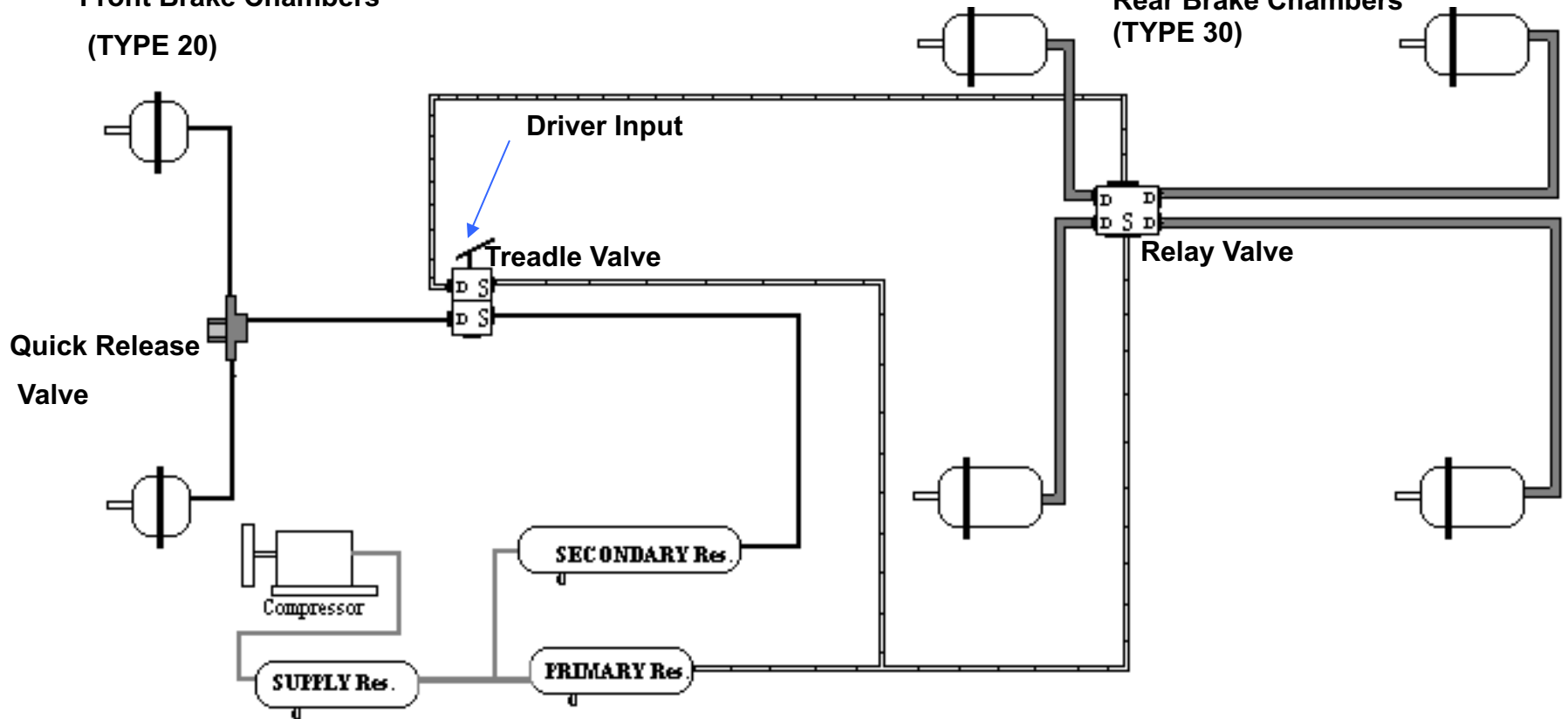
Quick Release  
Valve

Compressor

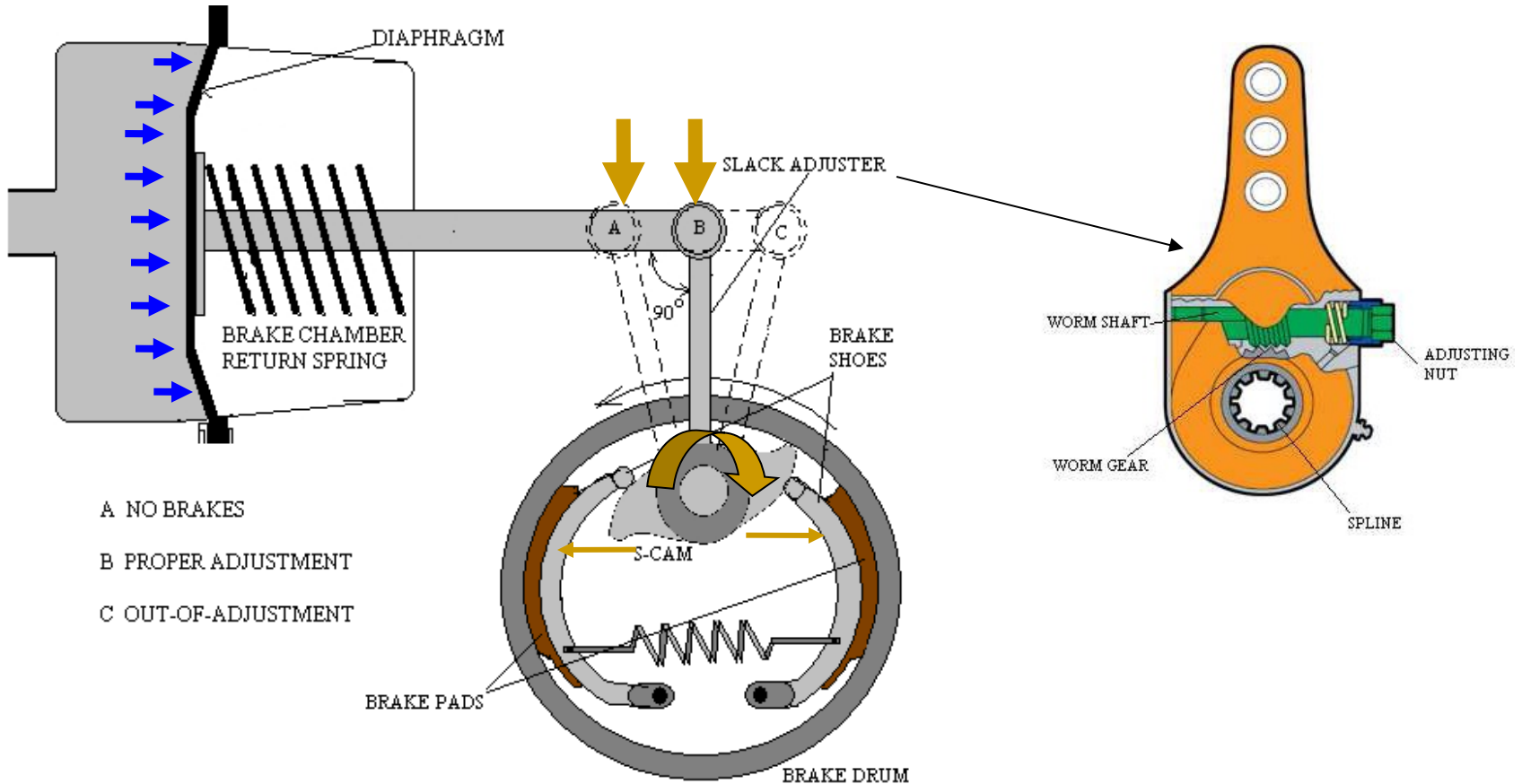
SUPPLY Res.

SECONDARY Res.

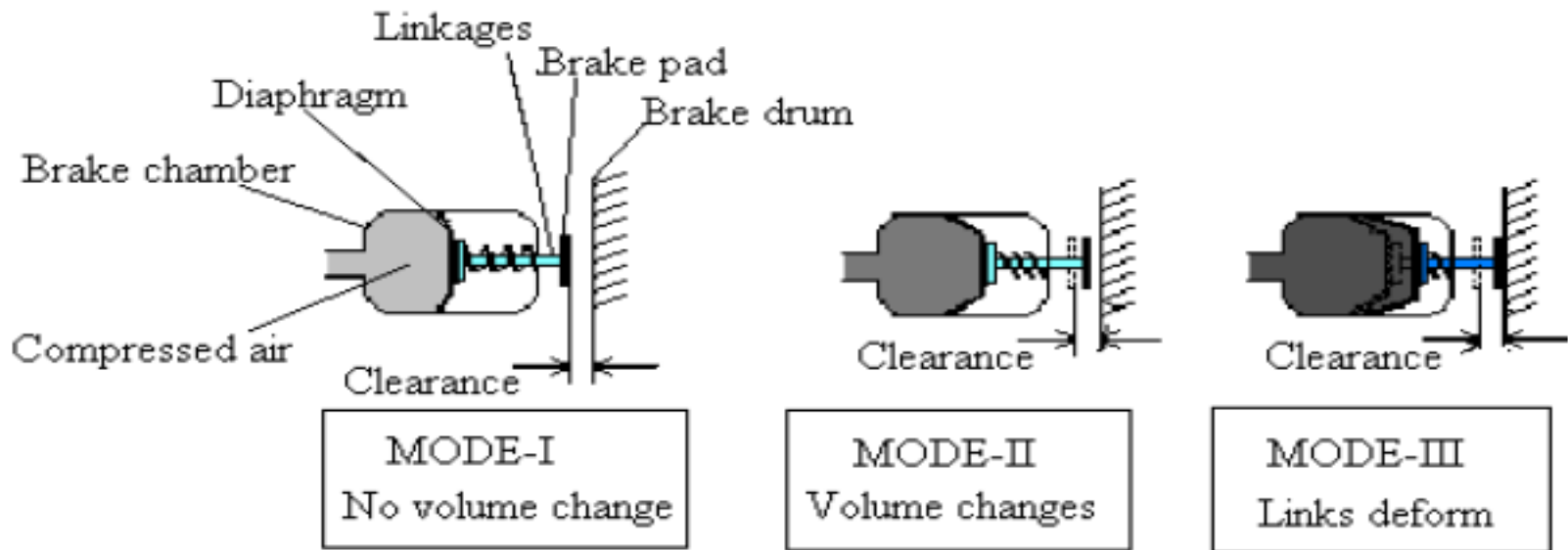
PRIMARY Res.



# Mechanical Subsystem



# Air Brake System a Hybrid System



# Main Issues for diagnostics of air brakes

- **Leakage of air**
  - **Affects the lag and maximum deceleration of the truck**
- **Pushrod stroke**
  - **Affects the volume available for air to expand → lag**
  - **Too much stroke → dead time in response**
  - **Stroke exceeds out-of-adjustment limit → braking force will be diminished**



# Out-of-adjustment of Pushrod

## ■ Causes of out-of-adjustment:

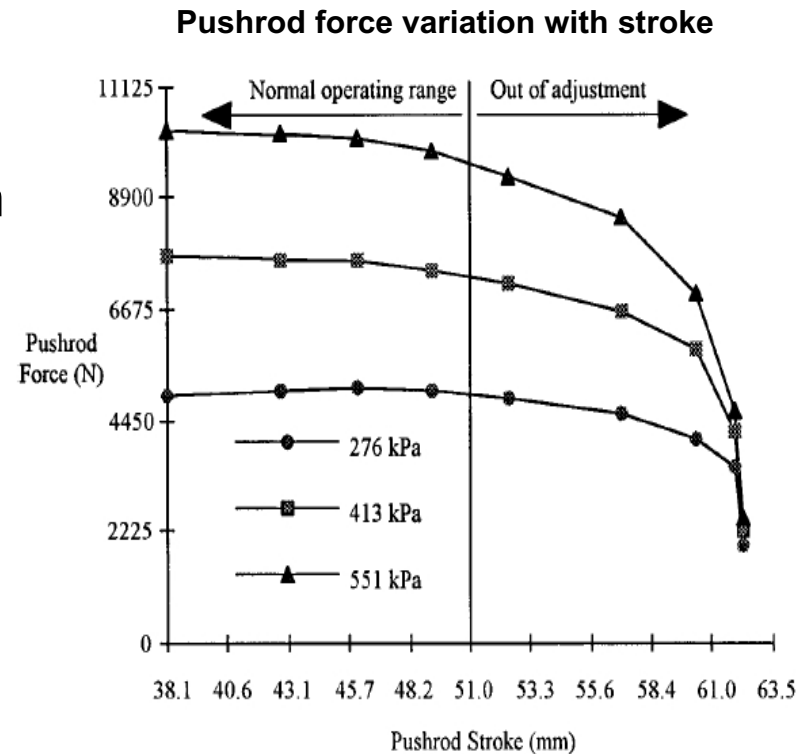
- Thermal expansion of brake drum
- Mechanical wear of brake pads

## ■ Effect:

- Kinematic misalignment
- Loss of braking force

## ■ Out-of-adjustment:

- If extension exceeds predefined safe limit (FMVSS 121)



# Existing Inspection Methods

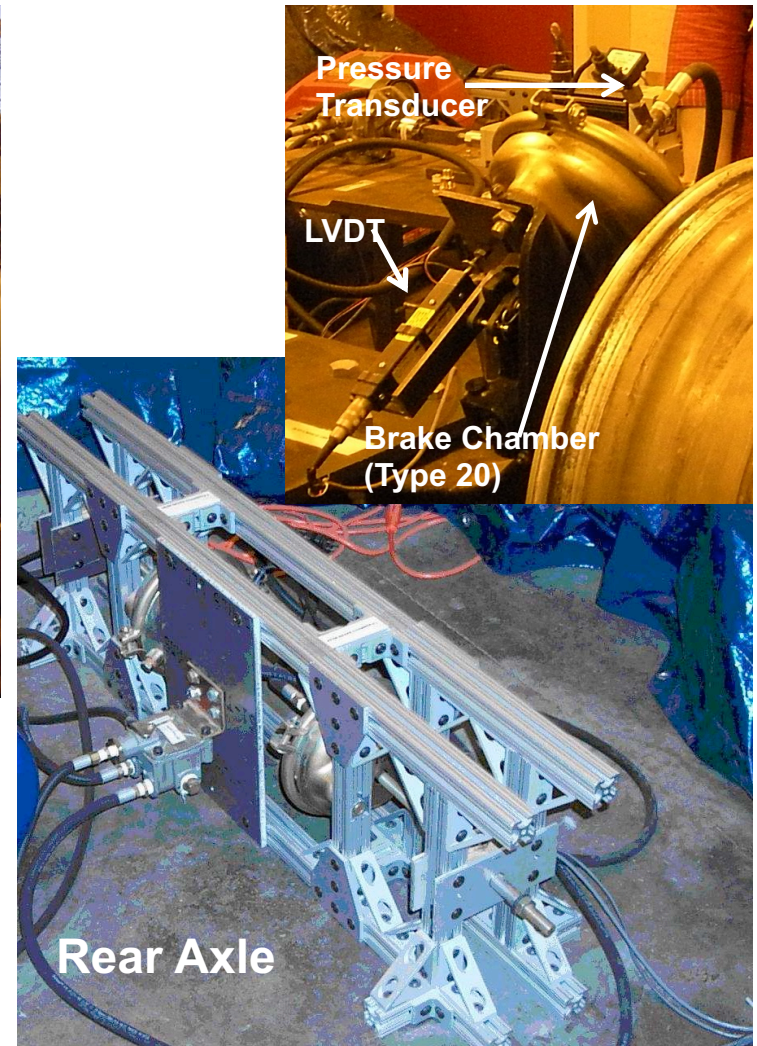
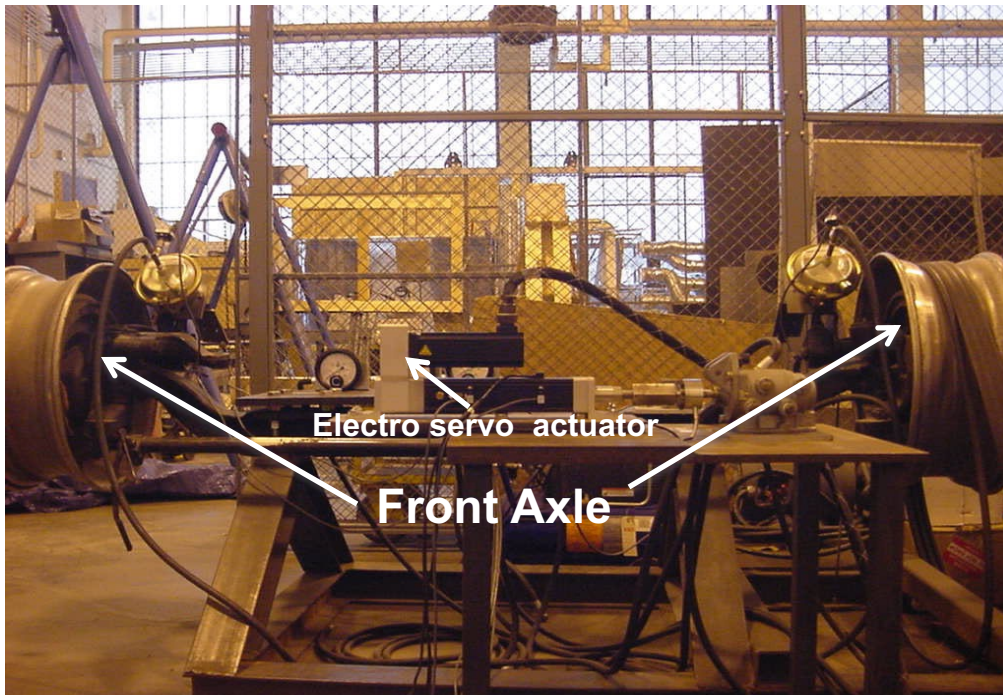
- **Manual Inspection (FMVSS 121)**
  - Labor intensive
  - Take 20 min. of 40 min. inspection time
- **Performance based inspection (FMCSR part 393)**
  - Roller dynamometers, Flat bed testers etc.
  - Measure max. deceleration / braking force
  - Transients not measured

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# Outline

- Introduction to Air Brakes
- Main issues for the development of diagnostic systems for air brakes
- *Experimental Setup at Texas A&M University*
- Basic idea for the estimation of Pushrod Stroke
- Conclusions

# Experimental Setup

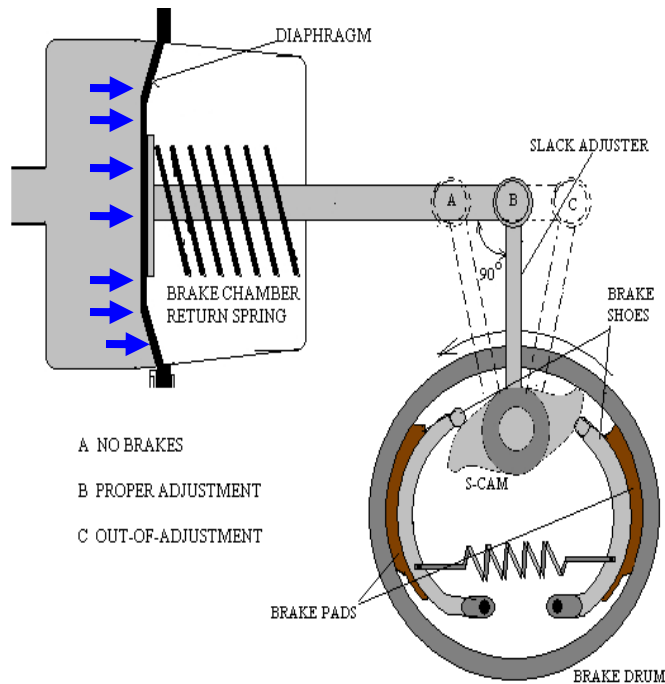


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# Outline

- Introduction to Air Brakes
- Main Issues for the diagnostics of air brakes
- Experimental Setup at Texas A&M University
- *Basic Idea for the estimation scheme*
- Conclusions

# Main Idea of Estimation



- **Measurements:** Pressure in the brake chamber when the brake pedal is fully applied.
- **Question:** What should the motion of the diaphragm be so that for the given mass flow rate of air entering the brake chamber, one would have the observed brake pressure?
- **Benefit:** Circumvents the hybrid nature of the problem and converts the problem to a standard nonlinear control problem
- **Method:** Once the motion of the diaphragm is known, one can estimate the stroke of the pushrod by numerical integration.

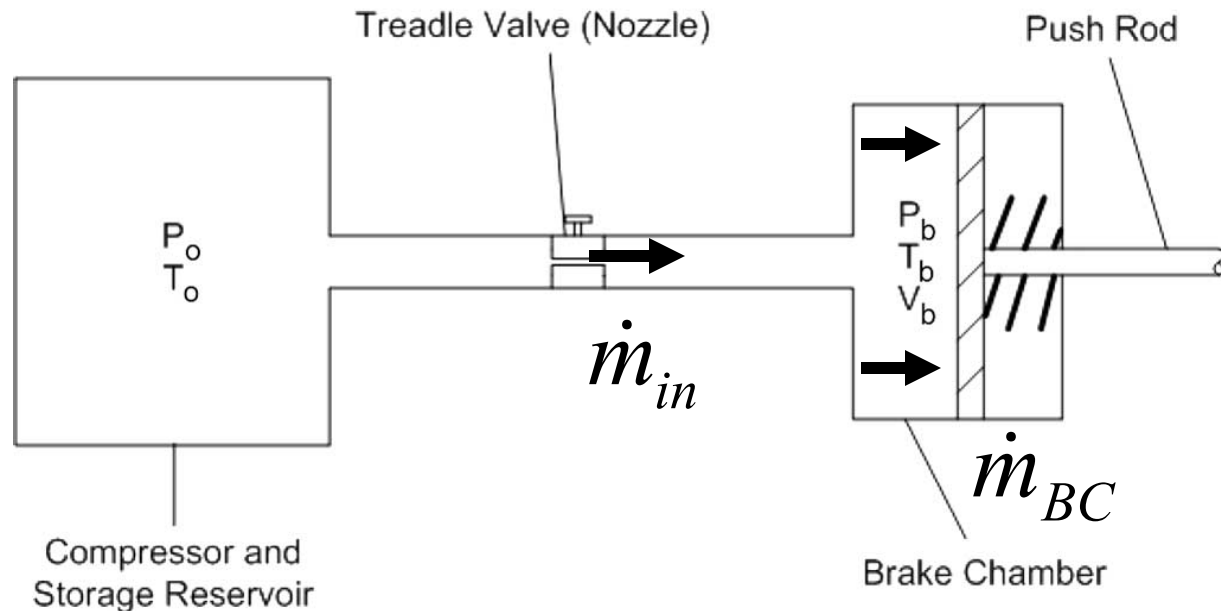
# Mathematical Model of Air Brake

## ■ Assumptions

- Lumped parameter approach
- Air behaves as ideal gas → all locations
- Treadle valve opening → a nozzle and varies.
- Isothermal process
- No frictional losses in hoses
- Compressibility effects ignored in hoses
- No leakage of air

# Mathematical Model of Air Brake

## Pneumatic Subsystem



$$\dot{m}_{in} = \dot{m}_{BC}$$



# Pressure Evolution Equation

- **Isothermal process**  $\dot{m}_{BC} = \frac{\dot{P}_b V_b + P_b \dot{V}_b}{RT_b}$

- **“Full-brake” application & isothermal process**

$$\therefore \dot{m}_{in} = \underbrace{A_P}_{fixed} P_b \underbrace{\sqrt{2RT \log\left(\frac{P_{sup}}{P_b}\right)}}_{u(P_b)}$$

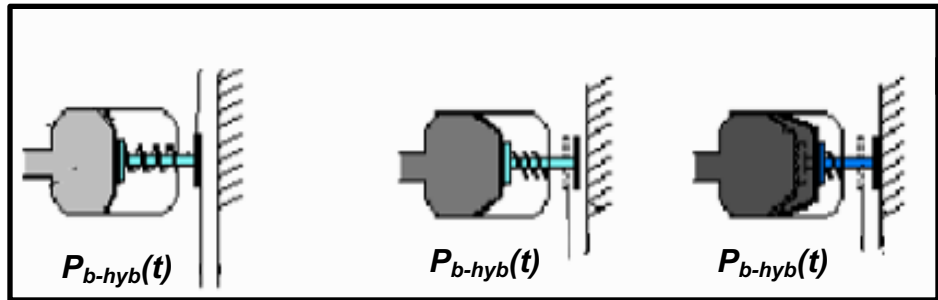
- **Volume varies with pushrod motion**

$$V_b(t) = V_i + A_b z(t) \quad \mathbf{Z} \rightarrow \text{Pushrod displacement}$$

- **Balance of mass  $\rightarrow \dot{m}_{in} = \dot{m}_{BC} \rightarrow$  evolution of pressure**

$$\dot{P}_b = \frac{A_P P_b \sqrt{2RT \log\left(\frac{P_{sup}}{P_b}\right)} - A_b P_b \dot{z}}{V_i + A_b z}$$

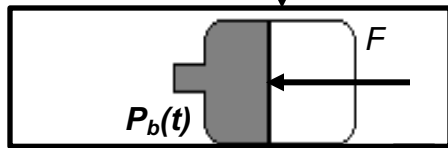
# Estimation Scheme



$$\dot{P}_{b-hyb} = f_A(P_{b-hyb}, z) + f_B(P_{b-hyb}, z)\dot{z}$$

$$\dot{z} = \begin{cases} g_1(P_{b-hyb}, z, K_1, C_1) & z \leq z_{cl} \\ g_2(P_{b-hyb}, z, K_2, C_2) & z > z_{cl} \end{cases}$$

$$y_m = P_{b-hyb}$$



$$\dot{P}_b = f_A(P_b, z) + f_B(P_b, z)F$$

$$\dot{z} = F$$

- Find  $F$  such that  $P_b(t)$  exactly tracks  $y_m(t)$

# Estimator for $z$

- For exact tracking  $\rightarrow P_b(t) = y_m(t) \rightarrow F$

$$F = \frac{1}{f_B(y_m, z)} [\dot{y}_m - f_A(y_m, z)]$$

- Estimator for  $z(T)$

$$\dot{z} = \frac{1}{f_B(y_m, z)} [\dot{y}_m - f_A(y_m, z)]$$

$$z(0) = z_0$$

# Estimation Scheme

- Assume  $y_m$  is smooth and noise free
- Assume internal dynamics are stable
- Tracking error  $e = P_b - y_m$
- Choose  $F$  such that
  - Exponential decay of tracking error
- $$F = \frac{1}{f_B(P_b, z)} \left[ \dot{y}_m - k_1(P_b - y_m) - f_A(P_b, z) \right]$$
- $K_1(>0)$  depends on desired rate of decay

# Governing Equations

$$\dot{P}_{b-hyb} = \underbrace{\frac{A_P P_{b-hyb} \sqrt{2RT \log\left(\frac{P_{sup}}{P_{b-hyb}}\right)}}{V_i + A_b z}}_{f_A(P_{b-hyb}, z)} + \underbrace{\left(\frac{-A_b P_{b-hyb}}{V_i + A_b z}\right)}_{f_B(P_{b-hyb}, z)} \dot{z}$$

} Pneumatic subsystem

$$\dot{z} = \begin{cases} g_1(P_{b-hyb}, z) & z \leq z_{cl} \\ g_2(P_{b-hyb}, z) & z > z_{cl} \end{cases}$$

} Mechanical subsystem

$$y_m = P_{b-hyb}$$

$z_{cl} \rightarrow$  clearance

$y_m \rightarrow$  measured output

# Estimation of $z$ with uncertainty in $A_p$

- $A_p$  varies with the type of valve (E-6, E-7, E-10)

- Assume uncertainty in  $A_p$

- The non hybrid system  $\dot{P}_b = \underbrace{A_p G_A(P_b, z)}_{f_A()} + f_B(P_b, z)F$

- Assume estimate of  $A_p$  known  $\dot{z} = F \rightarrow \hat{A}_p$

$$F = \frac{1}{f_B(P_b, z)} \left[ \dot{y}_m - k_1(P_b - y_m) - \hat{A}_p G_A(P_b, z) \right]$$

- Since  $\hat{A}_p \neq A_p \rightarrow$  error evolution  $\dot{e} + k_1 e = \tilde{A}_p G_A(P_b, z)$

- $\tilde{A}_p = A_p - \hat{A}_p$

# Estimation of $z$ with uncertainty in $A_p$

- Choose adaptation law for  $\hat{A}_p$

$$\dot{\hat{A}}_p = \Gamma(P_b - y_m)G_A(P_b, z)$$

$$\Gamma > 0$$

- Can be shown  $\rightarrow e \rightarrow 0$

- Estimator  $\dot{z} = \frac{1}{f_B(P_b, z)} \left[ \dot{y}_m - k_1(P_b - y_m) - \hat{A}_p G_A(P_b, z) \right]$

$$\dot{\hat{A}}_p = \Gamma(P_b - y_m)G_A(P_b, z)$$

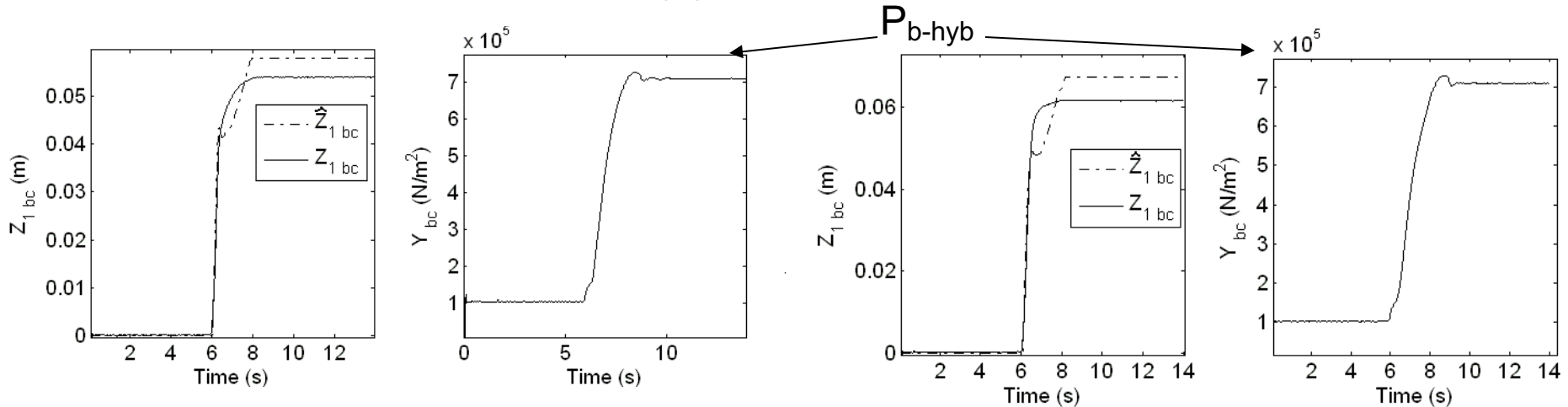
$$A_p(0) = A_{po}$$

$$z(0) = 0$$

# Experimental Corroboration

- Data for “full-brake” application
- Different strokes simulated
  - Changing pad-drum clearance → slack adj. nut

Estimate of  $z(T)$  for experimental data



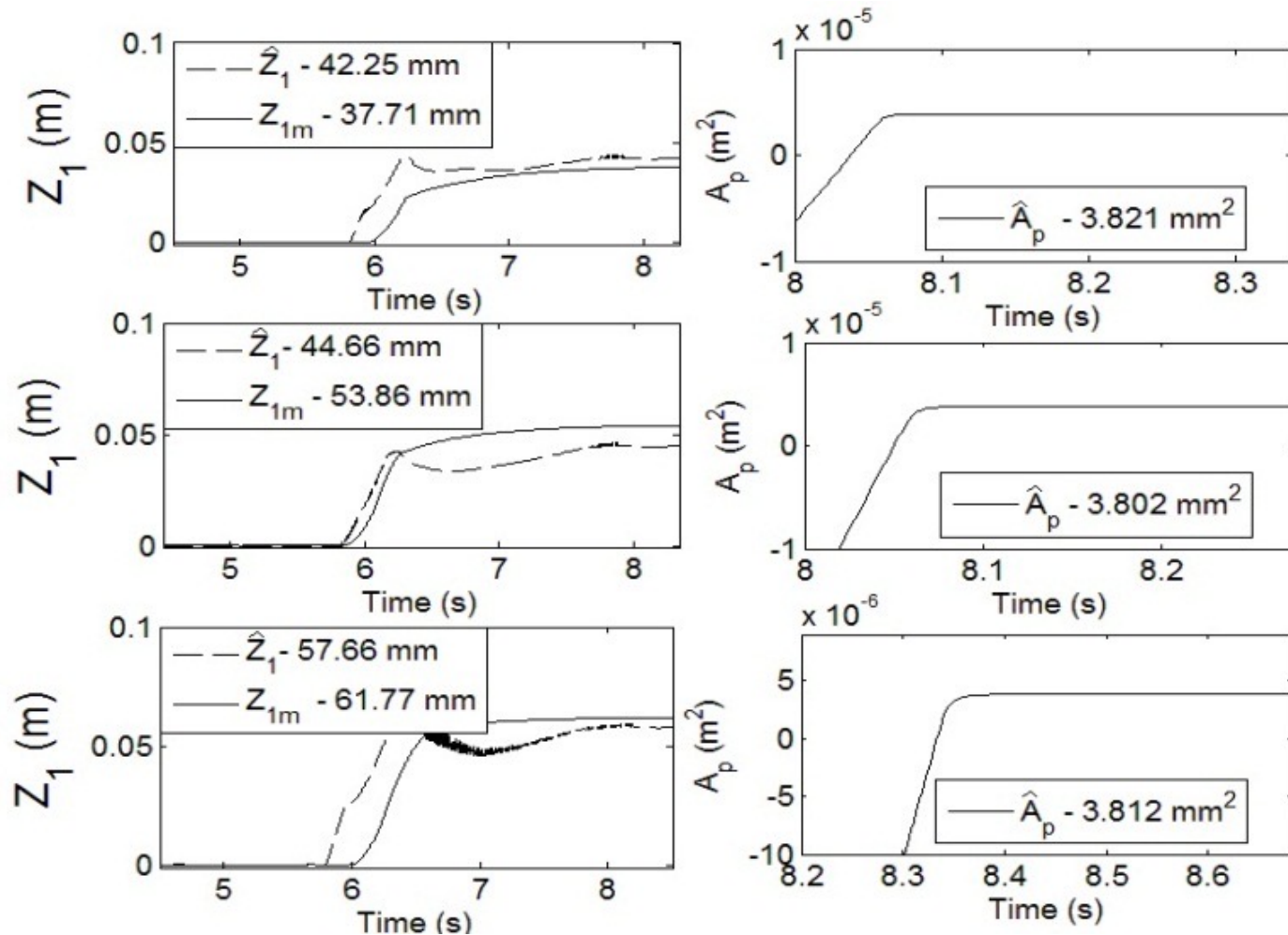
For  $z_{setup}(T) = 55 \text{ mm}$

For  $z_{setup}(T) = 61 \text{ mm}$



# Experimental Corroboration

Estimate of  $z$  &  $A_p$  for experimental data



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# Conclusions

- **Model based estimation of pushrod stroke**
  - **Controller design problem for non hybrid system**
  - **Non hybrid system obtained**
    - **Disconnecting hybrid part**
  - **Parameter estimation**
    - **Integrating equations for internal dynamics**
- **Schemes corroborated with test setup data**

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**Thank you**

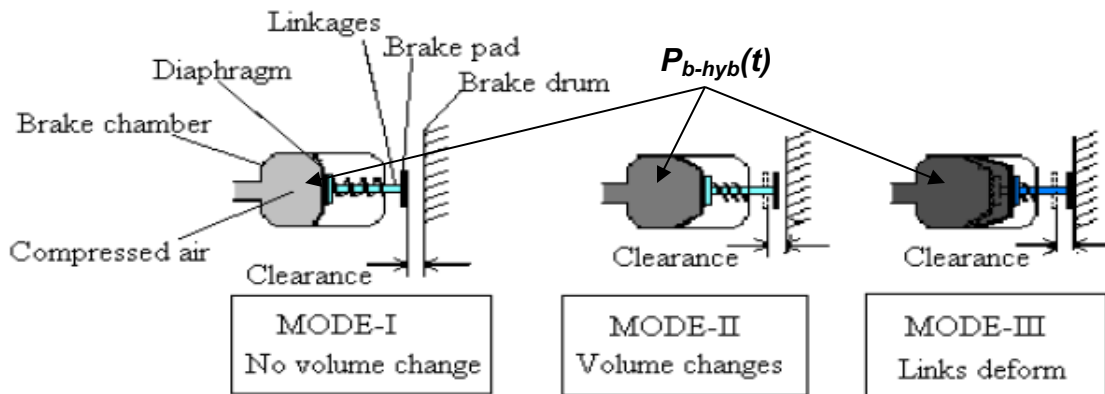
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**Questions ?**

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# Air Brake a Hybrid System

## ■ Mode dependent motion of pushrod

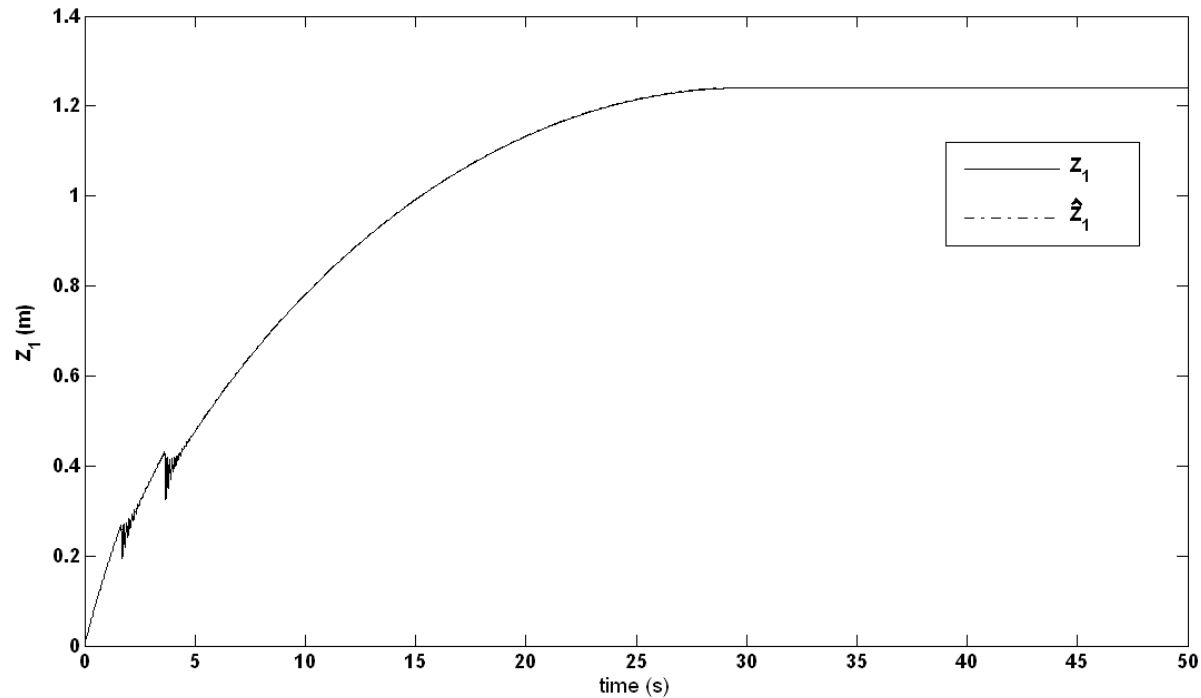


- Different governing equations in each mode
- Air Brake System → a hybrid system

# Estimation in Hybrid Systems

- **Mode to mode transition parameters**
  - Air brake system  $\rightarrow$  *clearance* ( $z_{cl}$ )
  
- **Parameters of system in each mode**
  - $\theta_i, i=\{1, 2\}$

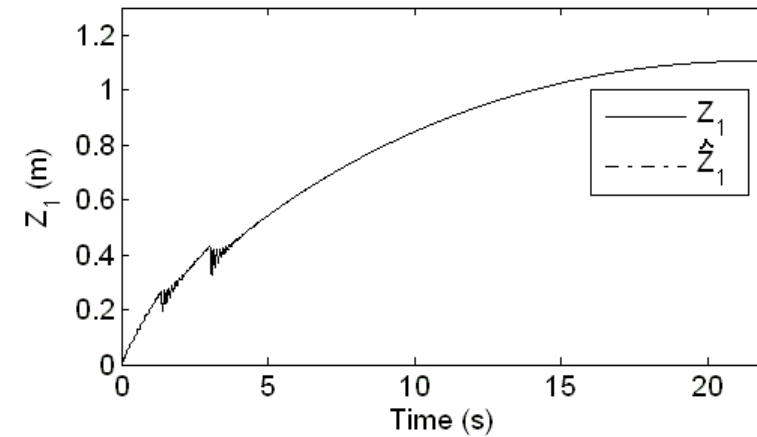
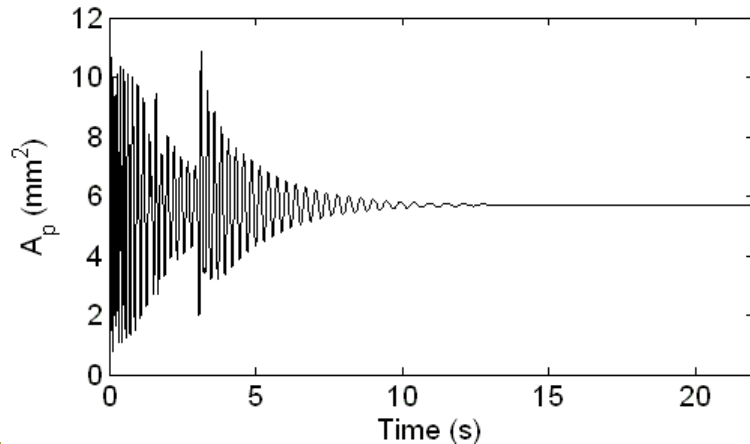
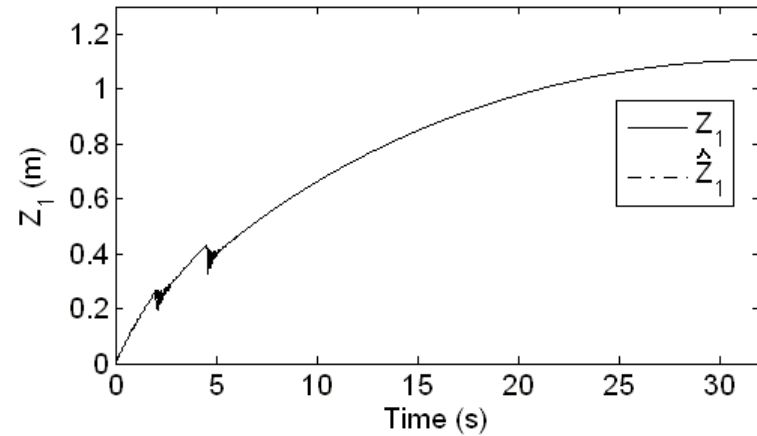
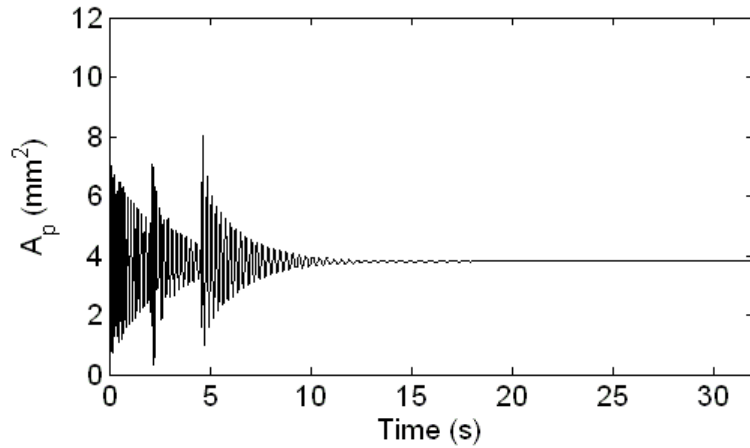
# Simulation Results



Estimate of  $z$  for simulated output of air brake system

# Simulation Results

Estimates of two different  $A_p$  for same supply pressure



# Problem of Estimation

- **Mode to mode transition parameters *not known***
  - $z_{c/}$  not known
- **Parameters of system in each mode *not known***
  - $\theta$
- **Uncertainty in parameters (valve area)**
- **Can one estimate the pushrod stroke in steady-state ?**



# Faults Affecting Air Brake System

- **26% of the reported crashes caused by brake faults**
- **Prominent faults (39.9%)**
  - **Out-of-adjustment of pushrod**
  - **Leakage of compressed air**

Source: LTCCS 2008 FMCSA US DoT

# Safety Devices On-board & Inspection

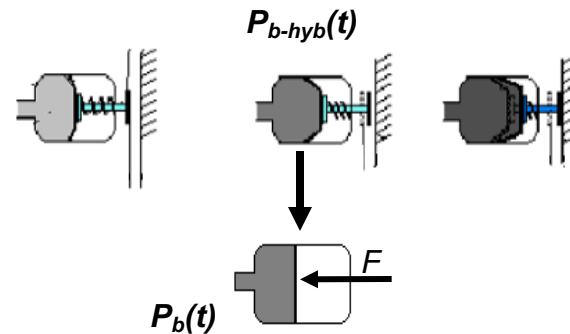
- **Out-of-adjustment of pushrod**
  - **Currently no on-board warning system**
  
- **Inspection of Out-of-adjustment of pushrod**
  - **“Full-brake” application @ 90psi**
  - **Measure steady-state stroke of pushrod**
  - **Compare with FMVSS 121**

# Practical Motivation

- **Diagnostic algorithms facilitating automated inspection**
  - To be implemented as
    - Hand-held device
    - On-board diagnostics
  
- **Estimate steady-state stroke of pushrod**
  - Uncertainty of area of opening of treadle valve (E-6, E-7, E-10)
  
- **Experimental implementation of the scheme**

# Advances to the state-of-art in hybrid systems

- Sequential hybrid systems
- Develop a parameter estimation scheme
  - Parametric uncertainty



- Seems to generalize for mechanical hybrid systems
- Experimental implementation